### **Laser Doppler Anemometry**

#### Introduction to principles and applications





### **Characteristics of LDA**

- Invented by Yeh and Cummins in 1964
- Velocity measurements in Fluid Dynamics (gas, liquid)
- Up to 3 velocity components
- Non-intrusive measurements (optical technique)
- Absolute measurement technique (no calibration required)
- Very high accuracy
- Very high spatial resolution due to small measurement volume
- Tracer particles are required



### **Applications of LDA**

- Laminar and turbulent flows
- Investigations on aerodynamics
- Supersonic flows
- Turbines, automotive etc.
- Liquid flows
- Surface velocity and vibration measurement
- Hot environments (Flames, Plasma etc.)
- Velocity of particles
- ..... etc, etc, etc.



### **LDA - Fringe Model**

- Focused Laser beams intersect and form the measurement volume
- Plane wave fronts: beam waist in the plane of intersection
- Interference in the plane of intersection
- Pattern of bright and dark stripes/planes





#### **Velocity = distance/time**



### **LDA - Fringe Model**

- The fringe model assumes as a way of visualization that the two intersecting beams form a fringe pattern of high and low intensity.
- When the particle traverses this fringe pattern the scattered light fluctuates in intensity with a frequency equal to the velocity of the particle divided by the fringe spacing.







### Laser, Characteristics and Requirements



### **Transmitting Optics**

#### **Basic modules:** Beam splitter BS Achromatic lens Laser Lens **Options:** Frequency shift (Bragg) Bragg cell) Ce - low velocities $D \times E$ $\times E$ - flow direction • Beam expanders 9 D - reduce measurement DL volume F - increase power density DAN

### **Receiving Systems**





### **System Configurations**



### **LDA Fibre Optical System**





### 60 mm and 85 mm FiberFlow probes





# The small integrated 3D FiberFlow probe





### **3-D LDA Applications**

- Measurements of boundary layer separation in wind tunnels
- Turbulent mixing and flame investigations in combustors
- Studies of boundary layer-wake interactions and instabilities in turbines
- Investigations of flow structure, heat transfer, and instabilities in heat exchangers
- Studies of convection and forced cooling in nuclear reactor models
- Measurements around ship models in towing tanks



### Seeding: ability to follow flow

Particle Frequency Response  $\frac{d}{dt}U_p = -18 \frac{\nu}{d_p^2} \frac{U_p - U_f}{\rho_p / \rho_f}$ 

| Particle         | Fluid                                 | Diameter (µm) |            |
|------------------|---------------------------------------|---------------|------------|
|                  |                                       | f = 1 kHz     | f = 10 kHz |
|                  |                                       |               |            |
| Silicone oil     | atmospheric air                       | 2.6           | 0.8        |
| TiO <sub>2</sub> | atmospheric air                       | 1.3           | 0.4        |
| MgO<br>8.8       | methane-air flame                     | 2.6           |            |
| TiO <sub>2</sub> | (1800 K)<br>oxygen plasma<br>(2800 K) | 3.2           | 0.8        |



### **Seeding: scattered light intensity**



- Polar plot of scattered light intensity versus scattering angle
- The intensity is shown on a logarithmic scale



## Measurement of air flow around a helicopter rotor model in a wind tunnel



Photo courtesy of University of Bristol, UK



## Measurement of water flow inside a pump model



Photo courtesy of Grundfos A/S, DK



# Measurement of velocity profiles in a water pipe





### Velocity profile, fully developed turbulent pipe flow





## Measurement of flow field around a 1:5 scale car model in a wind tunnel



Photo courtesy of Mercedes-Benz, Germany



## Measurement of wake flow around a ship model in a towing tank



Photo courtesy of Marin, the Netherlands



## Measurement of air flow field around a ship model in a wind tunnel



Photo courtesy of University of Bristol, UK



## Measurement of flow around a ship propeller in a cavitation tank





### **Comparison of EFD and CFD results**





### **Hot-Wire Anemometry**



• Purpose:

to measure mean and fluctuating variables in fluid flows (velocity, temperature, etc.): mean velocity, turbulence characteristics



### **CTA Application**

#### Flow field over helicopter landing pad



(Danish Maritime Institute, Lyngby Denmark)



### **Anemometer signal output**

The thermal anemometer provides an analogue output which represents the velocity in a point. A velocity information is thus available anytime.

Note that LDA signals occur at random, while PIV signals are timed with the frame grapping of illuminated particles.





### **Principles of operation**

• Consider a thin wire mounted to supports and exposed to a velocity *U*.

When a current is passed through wire, heat is generated  $(I^2R_w)$ . In equilibrium, this must be balanced by heat loss (primarily convective) to the surroundings.

 If velocity changes, convective heat transfer coefficient will change, wire temperature will change and eventually reach a new equilibrium.





### **Governing equation**

• Governing Equation:  $\frac{dE}{dt} = W - H$ 

E = thermal energy stored in wire E = CwTs Cw = heat capacity of wire W = power generated by Joule heating  $W = l^2 Rw$ recall Rw = Rw(Tw)H = heat transferred to surroundings



### Simplified static analysis I

• For equilibrium conditions the heat storage is zero:

$$\frac{dE}{dt} = O \quad \therefore W = H$$

and the Joule heating W equals the convective heat transfer H

#### Assumptions

- Radiation losses small
- Conduction to wire supports small
- Tw uniform over length of sensor
- Velocity impinges normally on wire, and is uniform over its entire length, and also small compared to sonic speed.
- Fluid temperature and density constant



### Simplified static analysis II

Static heat transfer:

 $W = H \implies I^2 Rw = hA(Tw - Ta) \implies I^2 Rw = Nukf/dA(Tw - Ta)$ 

- *h* = film coefficient of heat transfer
- A = heat transfer area
- *d* = wire diameter
- *kf* = heat conductivity of fluid
- Nu = dimensionless heat transfer coefficient

Forced convection regime, i.e.  $Re > Gr^{1/3}$  (0.02 in air) and  $Re < 140 \implies$ 

 $Nu = A_1 + B_1 \cdot Re^n = A_2 + B_2 \cdot U^n$  $I^2 Rw^2 = E^2 = (Tw - Ta)(A + B \cdot U^n)$  "King's law"

The voltage drop is used as a measure of velocity  $\Rightarrow$  data acquisition, processing

A, B, n: BY CALIBRATION



### **Directional response**

Probe coordinate system



Velocity vector *U* is decomposed into normal *Ux*, tangential *Uy* and binormal *Uz* components.



### **Probe types I**

- Miniature Wire Probes
  Platinum-plated tungsten,
  5 μm diameter, 1.2 mm length
- Gold-Plated Probes
  3 mm total wire length,
  1.25 mm active sensor
  copper ends, gold-plated

\_Advantages:

- \_- accurately defined sensing length
- reduced heat dissipation by the prongs
- more uniform temperature distribution along wire
- less probe interference to the flow field







### **Probe types II**

#### • Film Probes

Thin metal film (nickel) deposited on quartz body. Thin quartz layer protects metal film against corrosion, wear, physical damage, electrical action

#### • Fiber-Film Probes

"Hybrid" - film deposited on a thin wire-like quartz rod (fiber) "split fiber-film probes."







### **Probe types III**

- X-probes for 2D flows
  2 sensors perpendicular to each other. Measures within ±45°.
- Split-fiber probes for 2D flows
  2 film sensors opposite each other on a quartz cylinder. Measures within ±90°.
- Tri-axial probes for 3D flows
  3 sensors in an orthogonal system. Measures within 70° cone.







#### **Constant Temperature Anemometer CTA**

- Principle:
  Sensor resistance is kept constant by servo amplifier
- Advantages:
  - Easy to use
  - High frequency response
  - Low noise
  - Accepted standard
- Disadvantages:
  - More complex circuit





### **Velocity calibration (Static cal.)**

- Despite extensive work, no universal expression to describe heat transfer from hot wires and films exist.
- For all actual measurements, direct calibration of the anemometer is necessary.

### **Dynamic calibration**

 To calibrate the internal dynamics of the instrumentation (electronics etc.)



### Problem Sources Temperature Variations

- Fluctuating fluid temperature
- \_\_\_Heat transfer from the probe is proportional to the temperature difference between fluid and sensor.

$$E^2 = (Tw-Ta)(A + B \cdot U^n)$$

As *Ta* varies:

- heat transfer changes
- fluid properties change

TO BE HANDLED

