# 7. Principles of <br> Phase Doppler Anemometry 

Dantec Measurement Technology

http://www.dantecmt.com

## General features of PDA

- Extension of the LDA principle
- Simultaneous measurement of velocity (up to 3 components) and size of spherical particles as well as mass flux, concentration etc.
- First publication by Durst and Zaré in 1975
- First commercial instrument in 1984
- Non-intrusive measurement (optical technique), on-line and in-situ
- Absolute measurement technique (no calibration required)
- Very high accuracy
- Very high spatial resolution (small measurement volume)


## Preconditions for the application of PDA

- Optical access to the measurement area (usually from two directions)
- Sphericity of particles (droplets, bubbles, solids)
- Homogeneity of particle medium (slight inhomogeneities may be tolerated if the concentration of the inhomogeneities is low and if the size of the inhomogeneities is much smaller than the wavelength used)
- Refractive indices of the particle and the continuous medium must usually be known
- Particle size between ca. $0.5 \mu \mathrm{~m}$ and several millimeters
- Max. particle number concentration is limited

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## Principle setup of PDA

## Optical parameters of a PDA setup:

- Beam intersection angle $\theta$
- Scattering angle $\varphi$
- Elevation angle $\psi$
- Polarization (parallel or perpendicular to scattering plane)

- Shape and size of detector aperture


## Optical principle of PDA

- A particle scatters light from two incident laser beams
- Both scattered waves interfere in space and create a beat signal with a frequency which is proportional to the velocity of the particle
- Two detectors receive this signal with different phases
- The phase shift between these two signals is proportional to the diameter of the particle



## Phase relationships

The phase shift between two detectors is:
For reflection:

$$
\Phi=\frac{2 \pi d_{p}}{\lambda} \frac{\sin \theta \sin \psi}{\sqrt{2(1-\cos \theta \cos \psi \cos \phi)}}
$$

For 1st order refraction:

$$
\Phi=\frac{-2 \pi d_{p}}{\lambda} \frac{n_{r e l} \sin \theta \sin \psi}{\sqrt{2(1+\cos \theta \cos \psi \cos \phi)\left(1+n_{r e l}^{2}-n_{r e l} \sqrt{2(1+\cos \theta \cos \psi \cos \phi)}\right.}}
$$

No calibration constant is contained in these equations.

## Phase - diameter linearity

- A linear relationship between measured phase difference and particle diameter only exists, if the detector is positioned such that one light scattering mode dominates.
- Simultaneous detection of different scattering modes of comparable intensity leads to nonlinearities in the phase-diameter relationship.



## Dantec 57X40 FiberPDA



- Exchangeable aperture masks
- Up to three velocity components


## Applications

- Sprays and liquid atomization processes
-Water sprays
-Fuel-, diesel injection
-Paint coating
- Agricultural sprays
- Medical, pharmaceutical sprays
-Cosmetic sprays
- Powder production
-Spray drying
Liquid metal atomization
- Bubble dynamics
- Cavitation
- Aeration
-Multiphase mass transfer


## Automotive Fuel Injection



Photo: AVL, Graz, Austria

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## Nozzle Design



Photo: Gustav Schlick GmbH \& Co., Untersiemau, Germany
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## Aircraft Engine Fuel Injection



Photo: DLR, Institut für Antriebstechnik, Köln, Germany

## 9. Light sheet flow visualisation



Flow visualised in the vicinity of a cylinder. $\mathrm{Re}=2000$. Air bubbles in water. (Van Dyke: An Album of Fluid Motion, Parabolic Press, stanford, California, 1982)


Flow visualised in the vicinity of a cylinder. $\mathrm{Re}=10000$. Hydrogene bubbles in water. (Van Dyke: An Album of Fluid Motion, Parabolic Press, Stanford, California, 1982)


Flow visualised in a diffuser. Air bubbles in water. (Kaufmann, W.: Technische Hydro- und Aeromechanik, Springer Verlag, 1963)


Particle Tracking Velocimetry. Flow downstream of a cylinder. (Agui, J. C. A., Jimenez, J.: On the Performance of Particle Tracking. J Fluid Mechanics, pp. 447 - 468, 1987)

## 10. Particle Image Velocimetry (PIV)



Principle of PIV (Lecture note by Pap, E., Otto-Von-Guericke Universitaet Magdeburg, Institut für Strömungstechnik und Thermodynamik, Lehrstuhl für Strömungsmaschinen)


PIV arrangement with rotating mirror laser sheet generator (Lecture note by Pap, E., Otto-Von-Guericke Universitaet Magdeburg, Institut für Strömungstechnik und Thermodynamik, Lehrstuhl für Strömungsmaschinen)


Typical image originated from multipulse illumination


Summary of PIV http://www.dantecdynamics.com/piv/princip/index.html 8 DANTEC


Image 1 at time t1

$$
\bar{V}=\frac{\Delta x}{\Delta t} \quad \bar{\Delta} x=?
$$

Image 2


Image 2 at time t2

PIV Lecture_Notes, "Particle Image Velocimetry", University of WARWICK, Optical Engineering Laboratory (OEL)


Maximum cross-correlation between Image 1 \& Image 2

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PIV Lecture_Notes, "Particle Image Velocimetry", University of WARWICK, Optical Engineering Laboratory (OEL)

Radial pump simulation: comparison of simulated flow field and PIV data



PIV measurement (Otto-Von-Guericke Universitaet Magdeburg)


FLUENT simulation (Dept. of Fluid Mechanics, BME)

## FlowManager 3D-PIV (Stereo PIV)

- Theory of stereoscopic PIV
- Dantec 3D-PIV software
- Application example: 3D-PIV in an automotive wind tunnel (used as example through the slide show)


## Fundamentals of stereo vision



True 3D displacement ( $\Delta \mathbf{X}, \Delta \mathbf{Y}, \Delta Z$ ) is estimated from a pair of 2D displacements ( $\Delta x, \Delta y$ ) as seen from left and right camera respectively

## Left / Right 2D vector maps

Left \& Right camera images are recorded simultaneously.

Conventional PIV processing produce 2D vector maps representing the flow field as seen from left \& right.

The vector maps are re-sampled in points corresponding to the interrogation grid.

Combining left / right results, 3D velocities are estimated.


## 3D reconstruction

## Overlap area with interrogation grid



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